Chapter 72 Thermal Performance of Fly Ash Geopolymeric Mortars Containing Phase Change Materials

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This paper reports experimental results on the thermal performance of fly ash-based 6 geopolymeric mortars containing different percentages of phase change materials 7 (PCMs). These materials have a twofold eco-efficient positive impact. On one hand, 8 the geopolymeric mortar is based on industrial waste material. And on the other 9 hand, the mortars with PCM have the capacity to enhance the thermal performance 10 of the buildings. Several geopolymeric mortars with different PCM percentages 11 (10%, 20%, 30%) were studied for thermal conductivity and thermal energy storage. 12

1 Introduction

Climate change-related effects are associated mainly to the emissions of energy 14 sector [1]. This in turn is dependent on the population rise that will be responsible for 15 a very high increase of electricity demand [2]. The energy needs of the building 16 sector are expected to grow more than 70% [3]. The European Union adopted very 17 ambitious plans in order to tackle this paramount problem. The European Energy 18 Performance of Buildings Directive (EPBD) 2002/91/EC has [4] required that by the 19 end of 2018, all new buildings must have a nearly zero-energy consumption. The use 20 of innovative materials like PCMs will make it easier for this target to be met 21 [5]. These materials use chemical bonds to store or release heat thus allowing for a 22 reduction on the energy consumption. The capability to store or release thermal 23

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energy in these materials depends strongly on the heat storage capacity, thermal 24 conductivity, the melting temperature and the outdoor environment. Recently the use 25 of PCMs on OPC-based materials has merit increased attention [6-8]. Also 26 according to the Roadmap to a Resource Efficient Europe, all waste is to be managed 27 as a resource [9]. This is a very important goal concerning the circular economy and 28 zero-waste target [10]. Thus, materials that have the ability for the reuse of several 29 types of wastes such as geopolymers must receive a special attention on this context 30 [11]. This includes waste like fly ash because they are generated in high amount 31 [12]. In this context this paper reports experimental results on the thermal perfor-32 mance of fly ash geopolymeric mortars containing PCMs because this is a research 33 line that so far has received little attention. 34

35 2 Experimental Programme

The binder precursor was composed by 90% of fly ash and 10% of calcium 36 hydroxide. Solid sodium hydroxide, which was obtained from commercially avail-37 able product of Ercos, SA, Spain, was used to prepare the 12M NaOH solution. The 38 chemical composition of the sodium hydroxide was 25%Na₂O and 75%H₂O. The 39 sodium silicate liquid was supplied by MARCANDE, Portugal. The chemical 40 composition of the sodium silicate was 13.5%Na₂O, 58.7% SiO₂ and 45.2% 41 H₂O. The fly ash was obtained from the PEGO Thermal Power Plant in Portugal, 42 and it was classified as class F according to ASTM-C618 standard [13]. It was used 43 as the base material for the production of the geopolymers. The chemical composi-44 tion of the fly ash is presented in Table 72.1. 45

Calcium hydroxide was supplied by LUSICAL H100 and contains more than 99% CaO. The sand was used as inert filler provided from the MIBAL, Minas de Barqueiros, SA, Portugal. The superplasticizer was commercially available in polyacrylate from Acronal series, with a density of 1050 kg.m³ from BASF. One type of organic microencapsulated PCM was considered: BSF26 with melting temperature of 26 °C. The properties of the selected PCM for this study are provided by the manufacturer and are presented in Table 72.2.

t1.2	SiO ₂	Al_2O_3	Fe ₂ O ₃	CaO	MgO	Na ₂ O	K ₂ O	TiO ₂
t1.3	60.8	22.7	7.6	1.0	2.2	1.5	2.7	1.5

t1.1 Table 72.1 Major oxides in fly ash (%)

t2.1 Table 72.2 Properties of PCMs

	Operating	T	3.6.1.1	A	Particle size
	temperature range	Latent heat of	Melting	Apparent density at	distribution range
t2.2	(°C)	fusion (J/g)	point (°C)	solid state (kg/m3)	(µm)
t2.3	10–30	110	26	350	5–90

AU2

The specimens were cured in laboratory conditions (25 °C and 65% relative 53 humidity (RH)). The thermal conductivities of the mortars were determined in four 54 representative measurements of each mortar formulation, using a steady-state heat 55 flow metre apparatus (ALAMBETA, Model Sensora), following recommendation of 56 ISO 8301:1991 [14]. Mortars were casted into cylinder moulds with diameter of 57 10 cm and length of 1 cm. Then thermal conductivity of the specimen is calculated 58 based on heat conduction heat transfer theory according to [15]. Specific enthalpies 59 of the mortars were determined using, it is relevant to submit the sample into the 60 differential scanning calorimeter-DSC testing (Model NETZSCH 200 F3 Maia) and 61 measure the corresponding heat fluxes at controlled environment. Based on this, the 62 specific heat as a function of temperature can be obtained, and the specific enthalpy 63 is determined. The DSC has an accuracy of ± 0.2 °C for temperature measurements. All the specimens were tested within aluminium crucibles with volume of 40 μ L 65 under nitrogen (N_2) atmosphere with a flow of 50 mL/min. The specimens were 66 weighted using analytical balance (model PerkinElmer AD-4) with accuracy of 67 ± 0.01 mg. Each specimen was sealed in the pan by using an encapsulating press. 68 An empty aluminium crucible was considered a reference in all measurements. A 69 heating/cooling rate of 5 °C/min was considered for all experiments. 70

3 Results and Discussion

The thermal conductivity results are presented in Table 72.3. The lowest thermal 72 conductivity is noticed for the mixtures based on a sodium silicate/sodium hydroxide 73 ratio of 2.5 and an activator/binder ratio of 0.7. For a similar activator/binder ratio, 74 the reduction of the sodium silicate/sodium hydroxide ratio to 2.0 leads to highest 75 results of thermal conductivity. Results show that the addition of PCM into the 76 different mortars results in a consistent reduction of thermal conductivities. The 77 highest reduction is noticed for the mixtures based on a sodium silicate/sodium 78 hydroxide ratio of 2.0 and an activator/binder ratio of 0.7. The DSC curves for the 79 testing of mortars at heating/cooling rate of 5 °C/min are shown in Fig. 72.1.

Formulations	Group name	Thermal conductivity (W/m. K)
12M_2.5S/H_0.8A/B	А	0.77
10PCM_12M_2.5S/H_0.8A/B	А	0.70
20PCM_12M_2.5S/H_0.8A/B	A	0.69
30PCM_12M_2.5S/H_0.8A/B	A	0.44
12M_2.5S/H_0.7A/B_1.0SP	В	0.52
10PCM_12M_2.5S/H_0.7A/B_1.5SP	В	0.47
20PCM_12M_2.5S/H_0.7A/B_1.5SP	В	0.44
30PCM_12M_2.5S/H_0.7A/B_1.5SP	В	0.42
12M_2.0S/H_0.7A/B_1.0SP	С	0.94
10PCM_12M_2.0S/H_0.7A/B_1.5SP	С	0.90
20PCM_12M_2.0S/H_0.7A/B_1.5SP	С	0.77
30PCM_12M_2.0S/H_0.7A/B_1.5SP_3.0 W	С	0.35

 Table 72.3
 Thermal conductivity of mortars

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t3.1

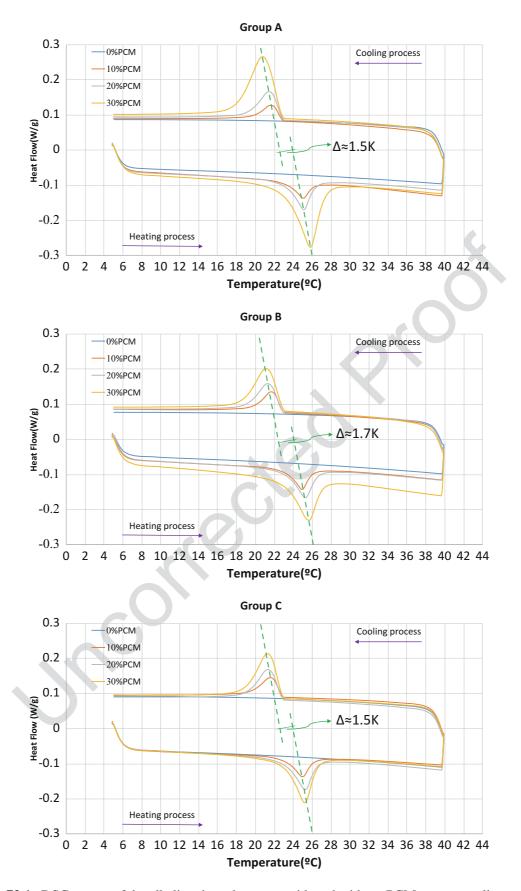


Fig. 72.1 DSC curves of the alkali-activated mortars with and without PCM upon a cooling and a heating cyclic test with a rate of 5 °C/min: (a) group A based on 12M_2.5S/H_0.8A/B; (b) group B based on 12M_2.5S/H_0.7A/B_1.0SP; (c) group C based on 12M_2.0S/H_0.7A/B_1.0SP

Overall, the results suggested that the PCM peak temperature shifts in the 81 direction of the imposed flux and further confirming higher peaks for mortars with 82 higher mass fraction of PCM into the mix. The two dashed lines per graphic have 83 been plotted by uniting the peak temperatures of all heating and all cooling thermo-84 grams: there is a clear linear relationship between the peak temperature of the 85 thermogram and the percentage of PCM embedded. When the two dashed lines for 86 a given group are compared, it can be noticed that they are approximately parallel 87 and that the distance between them ranges from $\Delta \approx 1.5$ K to $\Delta \approx 2.5$ K. The 88 difference observed in this hysteresis is known to depend on the internal thermal 89 gradients upon the tested sample, which tend to lag or raise heat exchange from 90 DSC. The average specific enthalpies for all the studied groups are ≈ 1.5 J/g, ≈ 2.5 J/ 91 g and ≈ 4 J/g for the mortar with 10%PCM, 20%PCM and 30%PCM, respectively. 92

4 Conclusions

The lowest thermal conductivity is noticed for the mixtures based on a sodium 94 silicate/sodium hydroxide ratio of 2.5 and an activator/binder ratio of 0.7. For a 95 similar activator/binder ratio, the reduction of the sodium silicate/sodium hydroxide 96 ratio to 2.0 leads to highest results of thermal conductivity. Results show that the 97 addition of PCMs results in a consistent reduction of thermal conductivities. The 98 average specific enthalpies for all the studied groups are ≈ 1.5 J/g, ≈ 2.5 J/g and ≈ 4 J/ 99 g for the mortar with 10%PCM, 20%PCM and 30%PCM, respectively.

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